

SPECIAL FEATURES OF THE COMPENSATION EFFECT IN NON-ISOTHERMAL KINETICS OF SOLID-PHASE REACTIONS

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(Received November 22, 1972)

The appearance of the compensation effect ($\log A = a + bE$) in non-isothermal kinetics of solid-phase reactions is discussed.

An analytical expression of the compensation effect is derived in the form

$$\ln A = \ln \frac{E \left(\frac{dT}{dt} \right)_s}{RT_s^2} + \frac{E}{RT_s}$$

It is demonstrated that the compensation effect appears in a number of chemical reactions if the T_s and rate constant values are close. Experimental data confirm the theoretical discussion.

In a number of chemical reactions whose rate constants are satisfactorily described by the Arrhenius equation

$$K = A \exp \left(\frac{-E}{RT} \right) \quad (1)$$

the so-called *compensation effect* [1] is sometimes observed:

$$\log A = a + bE \quad (2)$$

This effect is also known in isothermal decompositions of solid substances and in catalytic reactions. A more generalized inspection reveals the existence of an interrelationship between the changes in three quantities, namely A , E and ΔT , the temperature range in which the solid-state reaction proceeds at a measurable rate [2]. The linear relationship described by Eq. (2) is observed when changes in decomposition conditions (dispersity, pressure of the gaseous reaction product, etc.) do not result in a noticeable change of ΔT .

The value of a is usually close to zero [2].

Several explanations exist for the compensation effect observed in isothermal processes. Some researchers consider this effect apparent [3].

The appearance of the compensation effect in the kinetics of non-isothermal reactions has not yet been studied in detail.

The rate of a solid-state chemical transformation under non isothermal condi-

tions can be written for various process mechanisms (interface reactions, growth of nuclei, diffusion) in the form

$$\frac{d\alpha}{dt} = K(1 - \alpha)^n \quad (3)$$

where α is the conversion and n the formal order of the reaction. By combining Eq. (3) with the Arrhenius equation, we obtain

$$\frac{d\alpha}{dt} = A(1 - \alpha)^n \exp\left(\frac{-E}{RT}\right) \quad (4)$$

In all cases, the dependence of the conversion rate $\frac{d\alpha}{dt}$ on time t is expressed by a curve having a maximum at the temperature T_s ($\alpha = \alpha_s$). At the maximum

$$E = \frac{nRT_s^2 \left(\frac{d\alpha}{dt}\right)_s}{q_s(1 - \alpha_s)}$$

Let us substitute Eq. (4) for the point α_s into the above equation. After simple transformation, we arrive at the following expression for the rate constant:

$$K = \frac{E \left(\frac{dT}{dt}\right)_s (1 - \alpha_s)^{1-n}}{RT_s^2 \cdot n} \exp\left(\frac{E}{RT_s}\right) \exp\left(\frac{-E}{RT}\right) \quad (5)$$

The value of $\frac{dT}{dt}$ is close to the value of the heating rate q ($^{\circ}\text{C/sec}$).

In accordance with Eq. (5), the value of the preexponential factor is

$$A = \frac{E \left(\frac{dT}{dt}\right)_s (1 - \alpha_s)^{1-n}}{RT_s^2 \cdot n} \exp\left(\frac{E}{RT_s}\right) \quad (6)$$

Since $\frac{(1 - \alpha_s)^{1-n}}{n} \approx 1$ [4, 5], we finally obtain

$$A = \frac{E \left(\frac{dT}{dt}\right)_s}{RT_s^2} \exp\left(\frac{E}{RT_s}\right); \quad \ln A = \ln \frac{E \left(\frac{dT}{dt}\right)_s}{RT_s^2} + \frac{E}{RT_s} \quad (7)$$

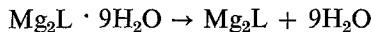
Eq. (7) is the analytical expression of the compensation effect for non-isothermal kinetics.

Thus, for a given substance, the compensation effect appears when $\left(\frac{dT}{dt}\right)$ a change in the decomposition conditions (dispersity, gas pressure) leads to a change in E , but to only a slight change in T_s .

This finding allows the treatment of the slight change in the value of T_s in non-isothermal kinetics as the basis of maintaining the constancy of the temperature range ΔT and the appearance of the compensation effect in isothermal kinetics.

For a number of chemical reactions, the compensation effect will be observed if $\left(\text{at } \frac{dT}{dt} = \text{const.}\right)$ the T_s values are close (leading to the constancy of b in Eq. (2) and the values of rate constants are close (ensuring the constancy of a in Eq. (2)).

By way of example for the first case, we shall consider the dehydration of the magnesium EDTA chelate:



This reaction was carried out in a continuous reactor (of the gas chromatograph type, fitted with a bypass instead of columns) allowing control of the rate of flow of nitrogen through the sample (10 mg) in an ampoule with a porous bottom. The results are presented in Table 1.

At low flow rates of the gas (~ 5 ml/min) the dehydration reaction (more precisely, the reversible deaquation and substitution of ligands) proceeds in an atmosphere of the released water vapour. At flow rates of ≥ 40 ml/min the dehydration conditions may be assumed to be close to the conditions of constantly maintained vacuum [6]. The change in the nitrogen flow rate will therefore change the shape of the kinetic curve, i.e. the value n of the formal order of reaction.

Table 1

Kinetic parameters of the dehydration of the magnesium EDTA chelate $\text{Mg}_2\text{L} \cdot 9\text{H}_2\text{O}$ ($q = 0.1$ °C/min) $\log A = 0.5 E - 3.5$

Parameters	Nitrogen flow rate, ml/min					
	6	10	15	20	25	40
T_s , K	448	423	409	420	418	398
n	0.75	1.1	1.2	1.5	1.9	2.0
E , kcal/mole	18.7	21.1	22.4	24.4	24.9	24.6
$\log A$	5.2	6.8	7.7	8.3	8.6	9.0

The compensation effect appears under the conditions of a corresponding increase of the effective energy of activation E on the increase of the formal order of reaction n . The curve $E = f(n)$ then proceeds close to the theoretically expected course [7, 8], corresponding to the formula $E_i \cdot \frac{1 - \alpha_{si}}{n_i \cdot \alpha_{si}} \approx E_0$, where E_0 is some definite minimum energy of activation of the chemical reaction for $n \rightarrow 0$. For endothermic processes corresponding to the scheme $A_s \rightarrow B_s + C_g$, the value of E_0 is close to the enthalpy of the process.

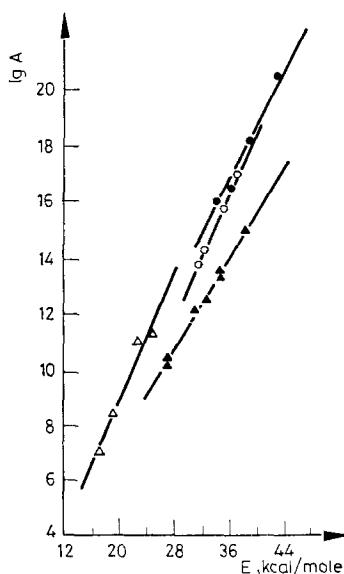


Fig. 1. Compensation effect in the dehydration of rare earth succinates and maleates: ○ — rare earth maleates; ● — lanthanum, cerium, erbium and ytterbium succinates; △ — praseodymium-holmium succinates (first dehydration stage); ▲ — praseodymium-holmium succinates (second dehydration stage)

By way of example for the second case, Fig. 1 illustrates calculations based on literature data [9, 10] for the dehydration of rare earth maleates and succinates having close values of T_s and rate constants.

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RÉSUMÉ — On discute l'apparition de l'effet de compensation ($\lg A = a + bE$) sur la cinétique non-isotherme des réactions en phase solide.

On propose une expression analytique de l'effet de compensation sous forme de l'équation

$$\ln A = \ln \frac{E \left(\frac{dT}{dt} \right)_s}{RT_s^2} + \frac{E}{RT_s}$$

On démontre que l'effet de compensation apparaît pour un certain nombre de réactions chimiques si les valeurs de T_s et des constantes de vitesse sont voisines. Des données d'expérience viennent à l'appui de la discussion théorique.

ZUSAMMENFASSUNG — Das Auftreten des Kompensationseffektes ($\lg A = a + bE$) in der nicht-isothermen Kinetik von Festphasenreaktionen wird erörtert.

Ein analytischer Ausdruck des Kompensationseffektes wird in Form der Gleichung

$$\ln A = \ln \frac{E \left(\frac{dT}{dt} \right)_s}{RT_s^2} + \frac{E}{RT_s}$$

abgeleitet.

Es wird bewiesen, daß der Kompensationseffekt bei einer Reihe von chemischen Reaktionen auftritt, wenn die Werte von T_s und die Geschwindigkeitskonstante nahe beieinander liegen. Versuchsanlagen bestätigen die theoretischen Erwägungen.

Резюме — Рассмотрено проявление «компенсационного эффекта» ($\lg A = a + bE$) в неизотермической кинетике твердофазных реакций.

Получено уравнение

$$\ln A = \ln \frac{E \left(\frac{dT}{dt} \right)_s}{RT_s^2} + \frac{E}{RT_s}$$

являющееся аналитическим выражением этого эффекта; показано, что компенсационный эффект наблюдается в случае близости величин T_s и констант скорости реакции у ряда химических реакций. Проведен эксперимент, подтверждающий теоретическое рассмотрение.